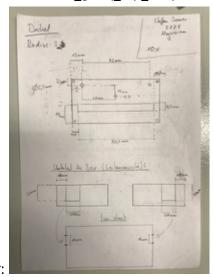
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Bake out

- We use the temperature monitoring design, made by E. Wodey, for the out of loop measurements during the out baking.
 - \circ Talk by E. Wodey for the explanation of the monitoring system: $2016\text{-}08_geoq_ctp_ew.pdf$



• Box-design made by S. Sauer:

Bake out list

Item	Material	Maximum temperature [°C]	Comments
CF Cupper ring	Cupper	1084.62	Schmelzpunkt, Wikipedia
Mounting for the spacer	(Al ~ Alplan)	660.2	
Zerodur rods	Zerodur	600	Wikipedia
Heat shields	Aluminium [EN AW-5083]	660.2	<fc #ff0000="">Temperatureinsatz (max. °C bei Dauer / Kurzzeiteinsatz): 120/ 180 </fc>
Screws from the mounting and hield shield	Edelstahl A2		
Window holder	Aluminium	660.2	
Vacuum chamber	Aluminium	660.2	
CF Flanschkit			
Glas balls	Borosilikatglas	500	maximale Arbeitstemperatur, Wikipedia
IGP		350	
Sub-D Socket			
CF-Kreuz			
Lead wire	Lead	327	
NTC Sensors		300	
Angle valve		< = 300	

temperature which the AR coatings are able to withstand? What is the maximum temperature gradient that can be applied (continuously) between the two faces of the 1/2" 3mm BK7 and fused silica windows Response from Jeremy at Thorlabs Windows 200 The maximum temperature will be around 200°C or so. We do not spe a maximum temperature gradient since it can depend on the thermal boundary conditions and geometrical boundary conditions on the window. However, I would recommend UVFS over N-BK7 because of its much lower coefficient of thermal coefficient. Vacuum glue [Torrseal] 175 Flammpunkt Indium wire Indium 155 Indium foil Indium 155	Item	Material	Maximum temperature [°C]	Comments
Sub-D Kabel 37FXRR-500 Kupferdraht versilbert 250 Vacuum pressure sensor Gate valve Cate valve Cosect: <= 200 Sub-D Feedthrough Crimp pins Cu vergoldet 200 Peltier-elements Question: What is the maximum (continuous temperature which the AR coating; are able to withstand? What is the maximum temperature wild the that can be applied (continuously) between the two faces of the 1/2" 3mm BK7 and fused silica windows Response from Jeremy at Thorlabs Windows Vacuum glue Torrseal] Indium wire Indium foil Indium sire lican dependent the two faces of the Indium 155 Indium wire Indium 155 Indium foil Indium sire Indium 155 Indium foil Indium sire Indium 155 Indium sire Indium 155	Capton wires			
Vacuum pressure sensor Z50 without electronics and magnet	Viton balls	Viton	280	Wikipedia
vacuum pressure sensor Gate valve Gate valve Sub-D Feedthrough Peek Crimp pins Cu vergoldet 230 IGP cable Peltier-elements Question: What is the maximum (continuous temperature which the AR coating are able to withstand? What is the maximum temperature gradient that can be applied (continuously) between the two faces of the 1/2" 3mm BK7 and fused silica windows Response from Jeremy at Thorlabs The maximum temperature gradient since it can depend on the therma boundary conditions on the window. However, I would recommend UVFS over N-BK7 because of its much lower coefficient of thermal coefficient. Vacuum glue [Torrseal] Indium wire Indium Institute Indium foil Indium 155 Indium foil Indium 155			250	
Gate valve (max 24h) closed: < = 200 Sub-D Feedthrough Peek 230 Crimp pins Cu vergoldet 230 Peltier-elements Question: What is the maximum (continuous temperature which the AR coating are able to withstand? What is the maximum temperature gradient that can be applied (continuously) between the two faces of the 1/2" 3mm BK7 and fused silica windows Response from Jeremy at Thorlabs The maximum temperature will be around 200°C or so. We do not spe a maximum temperature gradient since it can depend on the thermal boundary conditions and geometrical boundary conditions on the window. However, I would recommend UVFS over N-BK7 because of its much lower coefficient of thermal coefficient. Vacuum glue [Torrseal] Indium wire Indium Institute 155 Indium foil Indium 155	•		electronics and	
Crimp pins IGP cable Peltier-elements 200 Question: What is the maximum (continuous temperature which the AR coatings are able to withstand? What is the maximum temperature gradient that can be applied (continuously) between the two faces of the 1/2" 3mm BK7 and fused silica windows Response from Jeremy at Thorlabs The maximum temperature will be around 200°C or so. We do not spe a maximum temperature gradient since it can depend on the thermal boundary conditions and geometrical boundary conditions of the window. However, I would recommend UVFS over N-BK7 because of its much lower coefficient of thermal coefficient. Vacuum glue [Torrseal] Indium wire Indium foil Indium 155 Indium foil	Gate valve		(max 24h)	
IGP cable Peltier-elements 200 Question: What is the maximum (continuous temperature which the AR coatings are able to withstand? What is the maximum temperature gradient that can be applied (continuously) between the two faces of the 1/2" 3mm BK7 and fused silica windows Response from Jeremy at Thorlabs The maximum temperature will be around 200°C or so. We do not spea a maximum temperature gradient since it can depend on the thermal boundary conditions and geometrical boundary conditions on the window. However, I would recommend UVFS over N-BK7 because of its much lower coefficient of thermal coefficient. Vacuum glue [Torrseal] Indium wire Indium 155 Indium foil Indium 155 Indium foil	Sub-D Feedthrough	Peek	230	
Peltier-elements Question: What is the maximum (continuous temperature which the AR coatings are able to withstand? What is the maximum temperature gradient that can be applied (continuously) between the two faces of the 1/2" 3mm BK7 and fused silica windows Response from Jeremy at Thorlabs The maximum temperature will be around 200°C or so. We do not spea a maximum temperature gradient since it can depend on the thermal boundary conditions and geometrical boundary conditions on the window. However, I would recommend UVFS over N-BK7 because of its much lower coefficient of thermal coefficient. Vacuum glue	Crimp pins	Cu vergoldet	230	
Question: What is the maximum (continuous temperature which the AR coatings are able to withstand? What is the maximum temperature gradient that can be applied (continuously) between the two faces of the 1/2" 3mm BK7 and fused silica windows Response from Jeremy at Thorlabs The maximum temperature will be around 200°C or so. We do not spe a maximum temperature gradient since it can depend on the thermal boundary conditions and geometrical boundary conditions of the window. However, I would recommend UVFS over N-BK7 because of its much lower coefficient of thermal coefficient. Vacuum glue [Torrseal] Indium wire Indium Institute	IGP cable		< 220	
What is the maximum (continuous temperature which the AR coatings are able to withstand? What is the maximum temperature gradient that can be applied (continuously) between the two faces of the 1/2" 3mm BK7 and fused silica windows Response from Jeremy at Thorlabs The maximum temperature will be around 200°C or so. We do not spe a maximum temperature gradient since it can depend on the thermal boundary conditions and geometrical boundary conditions on the window. However, I would recommend UVFS over N-BK7 because of its much lower coefficient of thermal coefficient. Vacuum glue [Torrseal] Indium wire Indium Indium Indium Insi	Peltier-elements		200	
[Torrseal]173FlammpunktIndium wireIndium155Indium foilIndium155			200	What is the maximum (continuous) temperature which the AR coatings are able to withstand? What is the maximum temperature gradient that can be applied (continuously) between the two faces of the 1/2" 3mm BK7 and fused silica windows? Response from Jeremy at Thorlabs: The maximum temperature will be around 200°C or so. We do not spec a maximum temperature gradient since it can depend on the thermal boundary conditions and geometrical boundary conditions of the window. However, I would recommend UVFS over N-BK7 because of its much lower
Indium foil Indium 155			175	Flammpunkt
	Indium wire	Indium	155	
	Indium foil	Indium	155	
Vacuum pressure sensor cable ULE Spacer				

ULE Spacer	
Mirrors	
ULE rings	
Faraday rotator	I
Glue from faraday rotator	

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Bake out tips

http://vacuumtunes.co.uk/vtut1.html

3.3 Baking

Early workers baked systems only to about 200C which was effective in removing weakly bound surface water and hydrocarbon molecules. It was not long before it was discovered that baking to higher temperatures was required to remove more tightly bound species and the hydrogen diffusing from the bulk, both of which had the effect of limiting the ultimate system vacuum. The effectiveness of high temperature bakes is amply demonstrated for example by Calder and Lewin (1967), who showed that outgassing could be reduced to about E-16 mbar I/s cm2 by baking for 11 days at 300C or 1 hr only at 635C. Barton and Govier (1968), showed that baking new 18/18/1 stainless steel components at 450C in vacuo, with the exception of traces of hydrogen, successfully removes all gases resulting from the previous history . Interestingly these workers found that gas adsorbed at the surface of stainless steel on re-exposure to atmosphere could be remove by baking at this temperature for 2 to 3 hrs. If pressures only of the order of E-9 mbar were required then sufficient gas could be removed by a 12 hr bake at 200 to 300C; for some applications it is thus worthwhile to use a separate vacuum oven for baking new components at 450C thus avoiding the need for the main system to withstand high temperatures.

Santeler (1991), quotes early work by Aero Vac Corporation which gives valuable data on the effect of baking to different temperatures which is reproduced here below:

Outgassing rates in Torr I/s cm2

BAKING TIME

BAKING TEMP	20 hrs	40 hrs	100 hrs	200hrs
150C	6.3E-11	5.3E-11	2.8E-11	2.0E-11
250C	6.3E-12	5.3E-12	2.8E-12	2.0E-12
400C	4.0E-13	1.7E-13	1.0E-13	1.0E-13
500C	8.0E-15	8.0E-16	4.0E-17	8.0E-19

The data above bring home clearly the benefits of high baking temperatures and the diminishing returns from increasing baking time much beyond 20 hrs for baking temperatures up to 400C; at 500C the table shows that it is worthwhile to bake for as long as 200 hrs although one might legitimately question the unusually low value of 8.0E-19 torr l/s cm2 that is quoted. Recent work (Ishikawa, 1995; Ishikawa et al 1991; and Ishikawa and Odaka1990), confirms the values above for lower temperatures but indicates that surface treatments and raw material quality can improve these figures substantially, (section 3.2 above).

Bake out Protocol

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